

Some definitions

Mass density, ρ_i [kg/m^3]: The amount of species i in a unit volume.

Molar concentration; C_i [kmol/m^3]: The amount of mole of species i in a unit volume.

If M_i [kg/kmol] is the molar weight of species i , relation between ρ_i and C_i as follows: $\rho_i = M_i C_i$

ρ_i represents the mass of species i per unit volume of the mixture, then the mixture density,

$$\rho = \sum \rho_i \quad \text{and} \quad C = \sum C_i$$

The amount of species i in the mixture may also be quantified as

$$m_i = \frac{\rho_i}{\rho}$$

and its mole fraction as

$$x_i = \frac{C_i}{C}$$

Then it follows that $\sum m_i = 1$ and $\sum x_i = 1$

Having $M_i = \frac{\rho_i}{C_i}$ also leads $M = \frac{\rho}{C}$ for mixture

$$M = \frac{\rho}{C} = \sum \frac{M_i C_i}{C} = \sum x_i M_i \quad \text{also.}$$

Exercise 9.1 of A.F. Mills (Basic Heat and Mass Transfer)

Derive equations: $m_i = \frac{x_i M_i}{\sum x_j M_j}$ and $x_i = \frac{m_i / M_i}{\sum m_j / M_j} = m_i \frac{M_j}{M_i}$

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Fick law of diffusion

$$m_i = \frac{p_i}{\rho} = \frac{p_i}{\sum p_j} \quad \text{where } c_i = \frac{p_i}{M_i} \rightarrow p_i = c_i M_i$$

$$\bar{m}_i = \frac{c_i M_i}{\sum c_i M_i} = \frac{c_i M_i}{\sum c_i \sum M_i} = \frac{c_i}{c} \frac{M_i}{M} = \boxed{x_i \frac{M_i}{M}}$$

$$\boxed{x_i} = \frac{c_i}{c} = \frac{\left(\frac{p_i}{M_i}\right) \left(\frac{M}{\rho}\right)}{M_i} = \boxed{m_i \frac{M}{M_i}}$$

Fick law of diffusion

$$\boxed{J_i'' = -\rho D_{ij} \frac{dm_i}{dx}} \quad , \text{ kg/m}^2\text{s} : \text{ mass diffusion flux of species } i$$

$$J = J_i'' A \quad , D_{ij} : \text{ Binary diffusion coefficient}$$

To express in molar base; having $c_i = \frac{p_i}{M_i}$ and $c = \frac{p}{M}$

$$J_i'' = -\rho D_{ij} \frac{dm_i}{dx} = -\rho D_{ij} \frac{d \frac{p_i}{\rho}}{dx} = -D_{ij} \frac{dp_i}{dx}$$

$$= -\rho D_{ij} \frac{d \left(\frac{c_i M_i}{c M} \right)}{dx} = -\rho D_{ij} \frac{d \left(\frac{M_i}{M} x_i \right)}{dx}$$

$$= -\rho \frac{M_i}{M} D_{ij} \frac{dx_i}{dx}$$

$$\boxed{\frac{J_i''}{M_i}} = -c D_{ij} \frac{dx_i}{dx} \quad \left[\frac{\text{kg kmol}}{\text{s m}^2 \text{ kg}} \right]$$

$$\boxed{J_i^{''*}} = -c D_{ij} \frac{dx_i}{dx} \quad , \frac{\text{kmol}}{\text{m}^2\text{s}} \quad , \text{ Fick law in molar base}$$

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Fick law of diffusion

Permeability and Solubility:



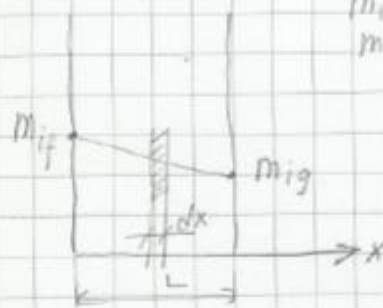
Solubility S : Volume of solute gas dissolved in unit volume of solid $[\text{kmol}/\text{m}^3 \cdot \text{bar}]$

$$C_{i, \text{solid side}} = S_{i, \text{solid}} \cdot P_{i, \text{gas side}}$$

Permeability $P_{i,s} = S_{i,s} \cdot D_{ij}$ ($\text{kmol}/\text{m}\cdot\text{s}\cdot\text{bar}$)

Then Fick's law interpretation in this concept;

Now let consider a plane wall;



m_{if} : Mass fraction in liquid side
 m_{ig} : " " " " gas side

$$J_i'' = -\rho D_{ij} \frac{dm_i}{dx} = \rho D_{ij} \frac{m_{if} - m_{ig}}{L} \quad \text{kg/s}\cdot\text{m}^2$$

or in mol fraction base

$$J_i'' = C D_{ij} \frac{X_{i1} - X_{i2}}{L}$$

As solid is in between two gas mixture, the concentration of component of the gas in the solid is proportional with with the partial pressure of the adjacent gas;

$$C_{i,s} = S_{ij} P_{i,g}$$

L solubility of i into j (kmol/m³.bar)

Solubility is related with diffusivity via permeability as

$$P_{ij} = S_{ij} D_{ij} \text{ [kmol/m.s.bar] : Permeability}$$

Substituting these into the molar Fick law, one can obtain the equation as follows:

$$j_i'' = C D_{ij} \frac{X_{i1} - X_{i2}}{L} = \cancel{C} \frac{D_{ij} C_{i1} - C_{i2}}{L} = D_{ij} \frac{C_{i1} - C_{i2}}{L}$$

Replacing C_{i1} & C_{i2} with $S_{ij} P_i$

$$j_i'' = S_{ij} D_{ij} \frac{P_{i1} - P_{i2}}{L} \quad \left[\text{where } P_{i1} \text{ and } P_{i2} \text{ are partial pressures of } i \text{ at 1. \& 2. regions -} \right.$$

or having $P_{ij} = S_{ij} D_{ij}$

$$j_i'' = P_{ij} \frac{P_{i1} - P_{i2}}{L}, \text{ kmol/m}^2.\text{s}$$

Another form of Fick's law may be expressed for the ideal gases as

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Fick law of diffusion

Example problem:

Hydrogen gas is maintained at 3 bar and 1 bar on opposite sides of a plastic membrane which is 0,3mm thick. The temperature is 25°C, and the binary diffusion coefficient of hydrogen in the plastic is $8 \times 10^{-8} \text{ m}^2/\text{s}$. The solubility of hydrogen in the membrane is $1.5 \times 10^{-3} \text{ kmol/m}^3 \cdot \text{bar}$. What is the mass diffusion flux of hydrogen through

the membrane?

$D_{\text{H}_2-\text{pls}} = 8 \cdot 10^{-8} \frac{\text{m}^2}{\text{s}}$, $S_{\text{H}_2-\text{pls}} = 1.5 \times 10^{-3} \text{ kmol/m}^3 \cdot \text{bar}$

$P_{\text{H}_2,1} = 3 \text{ bar}$ $P_{\text{H}_2,2} = 1 \text{ bar}$

$L = 0,0003 \text{ m}$

$J''_{\text{H}_2-\text{pls}} = P_{\text{H}_2-\text{pls}} \frac{P_{\text{H}_2,1} - P_{\text{H}_2,2}}{L}$

$= 13,05 \times 10^{-11} \frac{(3-1) \text{ bar} \cdot \text{kmol}}{\text{m}^2 \cdot \text{s} \cdot \text{bar}}$

$J''_{\text{H}_2-\text{pls}} = 8,7 \times 10^{-7} \frac{\text{kmol}}{\text{s} \cdot \text{m}^2}$

$P = 13,05 \times 10^{-11} \frac{\text{kmol}}{\text{m}^2 \cdot \text{s} \cdot \text{bar}}$

$R = S_{\text{H}_2-\text{pls}} \cdot P_{\text{H}_2,1} \cdot D_{\text{H}_2-\text{pls}}$

$= 8,7 \times 10^{-8} \frac{\text{m}^2}{\text{s}} \cdot 1,5 \times 10^{-3} \frac{\text{kmol}}{\text{m}^3 \cdot \text{bar}}$

$J''_{\text{H}_2-\text{pls}} = M_{\text{H}_2} \cdot J''_{\text{H}_2-\text{pls}}$

$= 2 \frac{\text{kg}}{\text{kmol}} \cdot 8,7 \times 10^{-7} \frac{\text{kmol}}{\text{s} \cdot \text{m}^2} = 1,74 \times 10^{-6} \text{ kg/s} \cdot \text{m}^2$

Some definitions on vapor air mixing

Relative humidity, $= \frac{m_v}{m_g}$,

Specific humidity, $\omega = \frac{m_v}{m_a}$

where

m_v : the vapor mass

m_g : the maximum vapor mass be able contained by the air at its existing temperature

m_a : air mass

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Fick law of diffusion

Using the ideal gas relation and recognizing that volume and temperature are shared by both vapor and air, we will have;

$$m_v = \frac{P_v V}{R_v T} \text{ and } m_a = \frac{P_a V}{R_a T}$$

Evaluating for specific humidity for $R_a = 287 \text{ J/kgK}$ and $R_v = 461 \text{ J/kgK}$

$$\omega = \frac{P_v \cancel{V} R_a \cancel{T}}{R_v \cancel{T} P_a \cancel{V}} = \frac{R_a P_v}{R_v P_a} = 0.622 \frac{P_v}{P_a} = \frac{0.622 x P_v}{P - P_v}$$

Since RH is also defined as $RH = \frac{P_v}{P_{sat@T}}$, then

$$\omega = \frac{0.622 x RH x P_{sat@T}}{P - P_{sat@T}}$$

Obtaining RH ,

$$RH = \frac{\omega x P}{(0.622 + \omega) P_{sat@T}}$$